

Surface Potential Model of Double Metal Fin Gate Tunnel FET

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Article Info

Page Number: 1044 – 1060

Publication Issue:

Vol. 71 No. 3 (2022)

Article History

Article Received: 12 January 2022

Revised: 25 February 2022

Accepted: 20 April 2022

Publication: 09 June 2022

Abstract

In this paper, we have proposed a surface model of double material Fin-shape gatetunnel FET (DM Fin TFET) analyzed based on a perimeter-weighted method for low voltage applications. The model obtained by the total device is separated into symmetrical and asymmetrical, and then solved by the 3D Poisson equation. The surface potential and the electrical field are obtained by solving the Poisson equation and the drain current is finally estimated using Kane's model to measure the tunneling generation rate. As compared with exiting model of single metal fin TFET is improved performance of the DM Fin-Gate TFET device i.e., enhanced ON-state current (I_{ON}), and low off-state current (I_{OFF}) and also improved the subthreshold swing(SS) of the proposed device. Our proposed model outputs are evaluated with TCAD device simulation software.

Keywords: Double-metal (DM) gate; FinTFET; Kane's tunneling model; surface potential, electric field,.

1 Introduction

To resolve the constraints of the MOS transistor, TFET has gained significant interest as an alternative device that likely reaches the nanometer dimensions of the MOSFET. The TFET is one of the most successful devices for minimum-consumption power i.e., Because of their least sub-threshold swing (SS) (even the minimum limit for standard MOS transistors is below 60 mV / decade) and low OFF-current. To enrichment of the electrostatic control and adequate ON/OFF performance is one of the most important factors. In these point of view traditional transistor architectures the same as the FinFET[1] are considered to be excellent solutions, because of FinFET has been proven possessing strong gate control ability[2]. These two device combinations are designed to achieve excellent performance. Researchers investigated a sum of possible strategies, for instance low band gap substances[3], metal gate work function, Source(S)/Drain(D) material engineering[4], strain channel engineering[5], high-k dielectric (or) partially mixture with SiO₂ Gate-oxide engineering[6], and multi-gate techniques[7] to enhance the TFETs drive current.

In this work, an effort has been made to report a 3-D analytical model for the asymmetrical doped channel of SOI based Fin Gate TFETs[8] with a dual gate oxide [9] structure. In this

direction, Kumar et al. suggested a double gate TFET with stacked gate oxide structure to reinforce the ON-current and diminish the SS value while retaining the unchanged OFF-state current value. The gate leakage current [10] could be considerably 6-7 orders reduced by replacement of SiO₂ /HfO₂ gate oxide structure. The need for a dual-material gate (DMG) consists of M₁ (close to source) and M₂ (close drain), with separate work functions, accordingly, ψ_{M1} and ψ_{M2} . For an n-type DMG device, $\psi_{M1} > \psi_{M2}$. In DMG system, the impact of the reduced electrical field in the drain side improves the gate control. The step potential indicates that the drain potential does not affect the potential under M₁. At the same point, the potential under M₂ is not controlled by the potential for drain. A high-K dielectric Gate Oxide double Material Fin structure TFET, device parameters along with surface potential and electrical fields addressed in this model. The Drain current is assessed using Kane band-to-band tunneling model [11] in TFET's. Finally, the effect of the different gate oxide thicknesses and the channel carrier doping concentrations [12] on the drain current also evaluated.

2. Working Mechanism of TFET:

The vital structure of tunnel FET has a p-i-n junction channel architecture. Figure 1. Shows the standard TFET device extremely doped with p⁺ region of the source, the intermediate doped of the n-type channel and also the highly doped n-type drain. Generally, TFET present includes different parameters like I_{GEN}, I_{BTBT} and I_s. I_{GEN} is generation current which is dependent upon the creation of holes and electrons at the depletion areas, is a part of reverse-biased voltage. I_{BTBT} is also band-to-band tunneling current which is dependent upon the tunneling of this carrier in the occupied band of this origin to an empty group of the station. I_s really is a reverse saturation current which is based on the diffusion part of the current.

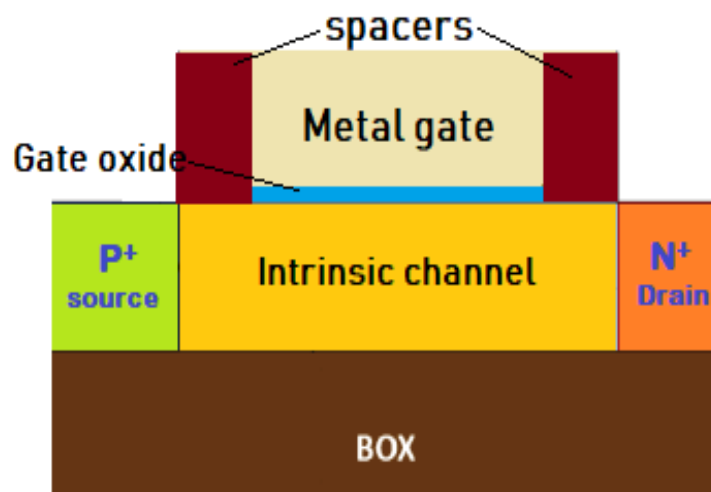


Figure 1. Schematic diagram of Tunnel FET structure.

I-V characteristics of TFET has two states one is OFF-state and another one ON state is shown in Figure 2. In this off-state gate is fully depleted the channel and also tunnel barrier length is very large because of small applied gate bias voltage. The leakage (I_{off}) current of the TFETs has very low (lower than the usual couple of pA/μm). In this ON state when the gate bias voltage exceed the threshold voltage gradually decrease barrier length and also flow

the conduction current (I_{on}) in between conduction and valance band of device. The gate bias exceeds beyond the limit in between band gap a path in the valence to conduction band will emerge near the source. The tunnel distance much reduced as compared to the amount of the intrinsic region and also an affected in BTBT and raises the conduction (I_{ON}) current of drain-source.

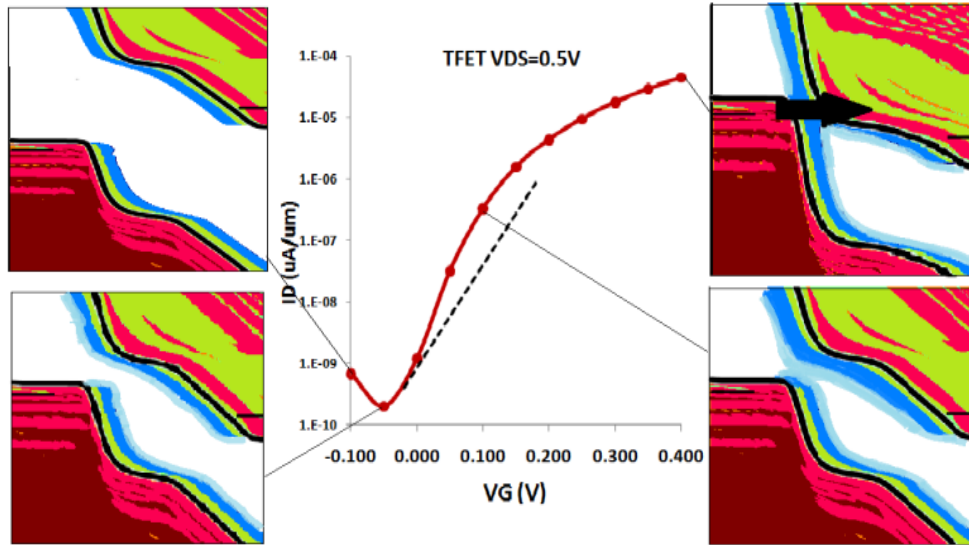


Figure 2. I-V characteristics with the different gate bias

2.1 Literaturesurvey

Kaishen Ou et al.[13] demonstrated structure for p-type Ge-Fin TFET with a wrapped around epitaxial layer is shown in Figure 3. The limitations are too large gate-source overlap can compromise drive current due to increased series resistance in the larger undoped epitaxial layer beneath the gate. Low temp. (330 ~ 400 °C) growth of Ge is preferred.

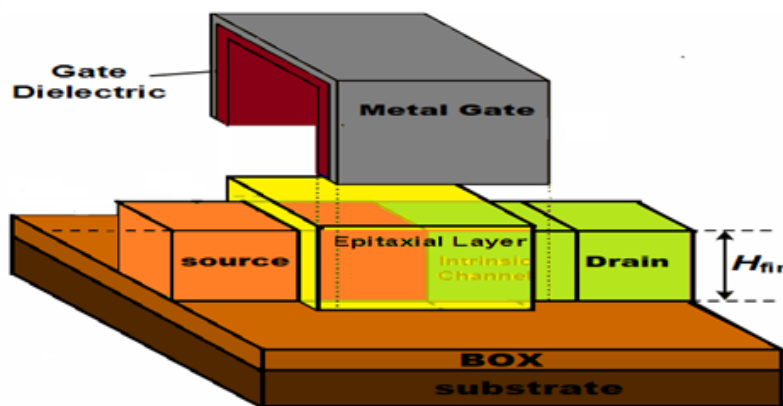


Figure 3. SiGe based FinTFET.

The influence of the height (H_{fin}) and width (W_{fin}) of a Si fin on the Epitaxial layer TFETs [13]. Because the EL is formed on the top and sidewall of a fin, the vertical BTBT cross-sectional area is proportional to H_{fin} . Therefore, the increase of H_{fin} leads to I_{on} boosting in the case of EL TFETs.

Priyanka Saha et al., [14] explained that Dual Metallic TG TFET will be It's been proven to research tunneling distance tuning from the station area by double gate dielectric with different values of work functions of metal 1&2 that BTB carrier tunneling at the origin into the station region enriches the BTB provider tunneling out of the origin to the station area with significant advancement in Ion/Ioff that the ratio will be 10^2 , the low threshold voltage.

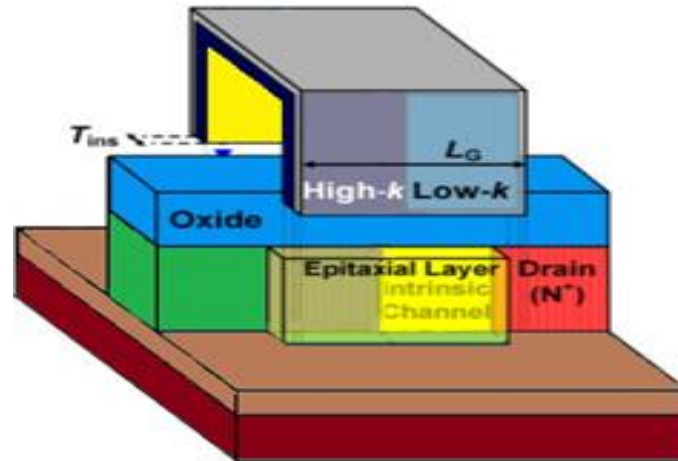


Figure 4. GHG TFET [15].

Jang Hyun Kim et al. [16] suggested TFET comes with a SiGe channel, a fin arrangement along with a raised drain to boost its electrical operation. It reveals I_{ON} is improved by twenty four times of silicon and six times more of silicon-germanium. The ambipolar current (I_{AMB}) can be decreased by 900 times compared with SiGe.

K.-H. Kao et al. [17], the fully overlapped device manufacture the high ON- currents, however. ON-current distinctions for the three types of TFET line tunneling. It in the main depends on supply concentration and Equivalent compound thickness (EOT) factors to decrease tunnel path.

3. Device Structure

A 3-D view of the DM Fin TFET structure is shown in Figure 6. The asymmetric intrinsic channel is highly doped with source side and lightly doped with drain side [18]. Two different gates M1 and M2 are utilized in the DM Fin-gate TFET [19], with the lengths L_1 and L_2 , correspondingly, and the total length of the gate is $L = L_1 + L_2$. A higher work function (ψ_{M1}) of L_1 is close to the source-end and lower work function (ψ_{M2}) of L_2 is adjacent to the drain-end performance as control and screening gate. The fin thickness is T_{si} and fin height is H_{fin} respectively.

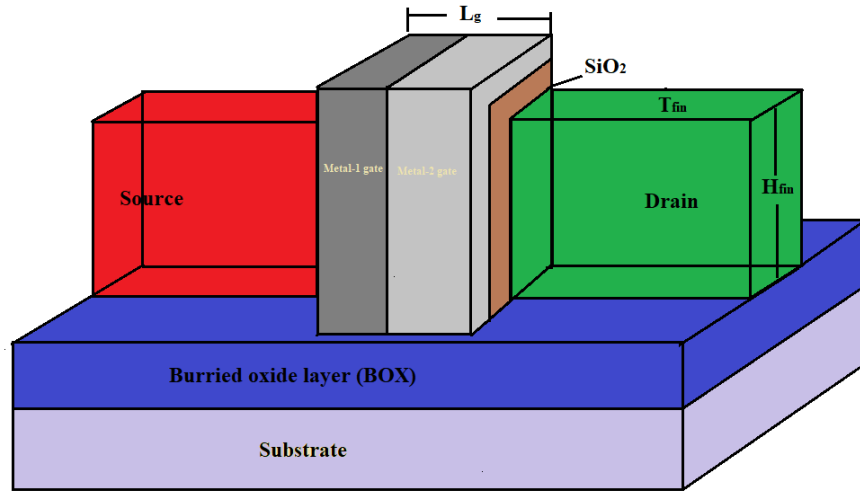


Figure 5. 3D view of the Double Metal Fin gate Tunnel FET

4. MODEL FORMATION

4.1 Surface Potential Model

The potential distribution inside the channel is attained by resolving 3D Poisson equation [20] with suitable constraints at the gate oxide interfaces and near source / drain ends. The total 3D structure separated into an asymmetric 2D device and symmetric 2D device .A 3D potential distribution is derived from perimeter-weighted sum method [21].

The 3D Poisson's condition along weak inversion region of channel can be express as:

$$\frac{\partial^2 \psi(x,y,z)}{\partial x^2} + \frac{\partial^2 \psi(x,y,z)}{\partial y^2} + \frac{\partial^2 \psi(x,y,z)}{\partial z^2} = \frac{qN_A}{\epsilon_{si}} ; 0 \leq x \leq T_{si} ; 0 \leq y \leq H_{fin} ; \text{ and } 0 \leq z \leq L, \quad (1)$$

Concept on initial conditions:

$$\psi_1(x, y, 0) = V_{bi,p} \quad (2)$$

$$\psi_2(x, y, L_1 + L_2) = V_{bi,n} + V_{ds} \quad (3)$$

Where $V_{bi,p} = -V_t \ln\left(\frac{N_a}{N_{ch}}\right)$; $V_{bi,n} = V_t \ln\left(\frac{N_d N_{ch}}{n_i^2}\right)$

Here the total length (L)=L₁+L₂and N_a, N_d are doping concentration of source side and drain side, 'V_t' is the thermal voltage and 'n_i' is the concentration of intrinsic carrier.

$$\left. \frac{d\psi_1(x,y,z)}{dy} \right|_{y=0} = \left(\frac{\epsilon_{ox}}{\epsilon_{si}} \right) \left(\frac{\psi_{s1}(x,0,z) - V'_{GS1}}{t_{ox}} \right); \quad (4)$$

$$\left. \frac{d\psi_2(x,y,z)}{dy} \right|_{y=0} = \left(\frac{\epsilon_{ox}}{\epsilon_{si}} \right) \left(\frac{\psi_{s2}(x,0,z) - V'_{GS2}}{t_{ox}} \right); \quad (5)$$

$$\left. \frac{d\psi_1(x,y,z)}{dy} \right|_{y=H_{fin}} = \left(\frac{\epsilon_{ox}}{\epsilon_{si}} \right) \left(\frac{V'_{SUB} - \psi_B(x,H_{fin},z)}{t_{oxb}} \right); \quad (6)$$

$$\left. \frac{d\psi_2(x,y,z)}{dy} \right|_{y=H_{fin}} = \left(\frac{\epsilon_{ox}}{\epsilon_{si}} \right) \left(\frac{V'_{SUB} - \psi_B(x,H_{fin},z)}{t_{oxb}} \right); \quad (7)$$

$$\left. \frac{d\psi_1(x,y,z)}{dy} \right|_{x=0} = \left(\frac{\epsilon_{ox}}{\epsilon_{si}} \right) \left(\frac{\psi_{s1}(0,y,z) - V'_{GS1}}{t_{ox}} \right); \quad (8)$$

$$\left. \frac{d\psi_2(x,y,z)}{dy} \right|_{x=0} = \left(\frac{\epsilon_{ox}}{\epsilon_{si}} \right) \left(\frac{\psi_{s2}(0,y,z) - V'_{GS2}}{t_{ox}} \right); \quad (9)$$

$$\left. \frac{d\psi_1(x,y,z)}{dy} \right|_{x=T_{si}} = \left(\frac{\epsilon_{ox}}{\epsilon_{si}} \right) \left(\frac{V'_{GS1} - \psi_{s1}(T_{si},y,z)}{t_{ox}} \right); \quad (10)$$

$$\left. \frac{d\psi_2(x,y,z)}{dy} \right|_{x=T_{si}} = \left(\frac{\epsilon_{ox}}{\epsilon_{si}} \right) \left(\frac{V'_{GS2} - \psi_{s2}(T_{si},y,z)}{t_{ox}} \right); \tag{11}$$

The potential distribution and electric fields in between two metals are continuous

$$\psi_1(x, y, L_1) = \psi_2(x, y, L_1); \tag{12}$$

$$\left. \frac{d\psi_1(x,y,z)}{dy} \right|_{z=L_1} = \left. \frac{d\psi_2(x,y,z)}{dy} \right|_{z=L_1}; \tag{13}$$

Where ψ is the total channel potential of ψ_1 and ψ_2 are the channel potential of M_1 and M_2 . ψ_{S1} and ψ_{S2} are the potential distribution of M_1 & M_2 respectively. ψ_b is the backend oxide conjunction with silicon interface potential, V_{ds} is the drain to source voltage and V_{bi} is the built in potential.

$$V'_{gs} = V_{gs} - V_{fb,f} \text{ and } V'_{sub} = V_{sub} - V_{fb,b},$$

Where V_{gs} , V_{sub} are the gate-source and substrate voltage, $V_{fb1,f}$ and $V_{fb2,f}$ are the front end channel flat-band potential for M_1 and M_2 , correspondingly, and $V_{fb,b}$ is the flatband potential of back end channel. Dual metal gate flat-band voltages V_{fb1} (or) ψ_{MS1} and V_{fb2} (or) ψ_{MS2} are specified as difference between potential of M_1 (or) M_2 and surface work function (ψ_s).

$$\text{work function of the semiconductor } (\psi_s) = \chi_{si} + \frac{E_g}{2q} + \psi_F \tag{14}$$

$$\text{Fermi potential } (\psi_F) = \psi_t \ln \left(\frac{N_a}{n_i} \right)$$

Where ψ_t is the thermal potential and χ_{si} is the electron affinity.

4.2 Potential for the asymmetric DM TFET

The asymmetric DM TFET potential distribution within the weak inversion region are often calculated by resolving the 2D Poisson equation [22], it's possible to write as

$$\frac{\partial^2 \psi(y,z)}{\partial y^2} + \frac{\partial^2 \psi(y,z)}{\partial z^2} = \frac{qN_a}{\epsilon_{si}}, \quad 0 \leq Y \leq H_{fin}, \quad 0 \leq Z \leq L \tag{15}$$

With boundary conditions

$$\left. \frac{d\psi_1(y,z)}{dy} \right|_{y=0} = \left(\frac{\epsilon_{ox}}{\epsilon_{si}} \right) \left(\frac{\psi_{s1}(z) - V'_{gs1}}{t_{ox}} \right); \tag{16}$$

$$\left. \frac{d\psi_2(y,z)}{dy} \right|_{y=0} = \left(\frac{\epsilon_{ox}}{\epsilon_{si}} \right) \left(\frac{\psi_{s2}(z) - V'_{gs2}}{t_{ox}} \right); \tag{17}$$

$$\left. \frac{d\psi_1(y,z)}{dy} \right|_{y=H_{fin}} = \left(\frac{\epsilon_{ox}}{\epsilon_{si}} \right) \left(\frac{V'_{sub} - \psi_b(z)}{t_{oxb}} \right); \tag{18}$$

$$\left. \frac{d\psi_2(y,z)}{dy} \right|_{y=H_{fin}} = \left(\frac{\epsilon_{ox}}{\epsilon_{si}} \right) \left(\frac{V'_{sub} - \psi_b(z)}{t_{oxb}} \right); \tag{19}$$

$$\psi_1(0, L_1) = \psi_2(0, L_1) \tag{20}$$

$$\left. \frac{d\psi_1(y,z)}{dz} \right|_{z=L_1} = \left. \frac{d\psi_2(y,z)}{dz} \right|_{z=L_1} \tag{21}$$

$$\psi_1(0, 0) = \psi_{S1}(0) = V_{bi,p} \tag{22}$$

$$\psi_2(0, L_1 + L_2) = \psi_{S2}(L_1 + L_2) = V_{bi,n} + V_{ds} \tag{23}$$

The potential distribution function in the perpendicular 'y' direction presumed as parabolic by giving the Young method[23]:

$$\psi_i(y, z) = \psi_{si}(z) + p_{i1}(z)y + p_{i2}(z)y^2, \tag{24}$$

Where $i=1,2$ and $p_{i1}(z)$ and $p_{i2}(z)$ are coefficients of z only.

For the DM model, the potential distribution of M_1 and M_2 are given by:

$$\psi_1(y, z) = \psi_{s1}(z) + p_{11}(z)y + p_{12}(z)y^2; \quad 0 \leq y \leq H_{fin}, \quad 0 \leq z \leq L_1 \tag{25}$$

$$\psi_2(y, z) = \psi_{s2}(z) + p_{21}(z)y + p_{22}(z)y^2 ; 0 \leq y \leq H_{fin}, L_1 \leq z \leq L_1 + L_2 \quad (26)$$

Put on the boundary conditions (16) to (19), we get the coefficients:

$$P_{11}(z) = \frac{C_{ox}}{\epsilon_{si}} (\psi_{s1}(z) - V'_{gs1}); \quad (27)$$

$$P_{21}(z) = \frac{C_{ox}}{\epsilon_{si}} (\psi_{s2}(z) - V'_{gs2}); \quad (28)$$

$$P_{12}(z) = \frac{[V'_{sub} - (1 + \frac{C_{ox}}{C_{oxb}} + \frac{C_{ox}}{C_{si}})\psi_{s1}(z) + (\frac{C_{ox}}{C_{oxb}} + \frac{C_{ox}}{C_{si}})V'_{gs1}]}{[1 + \frac{2C_{si}}{C_{oxb}}]H_{fin}}; \quad (29)$$

$$P_{22}(z) = \frac{[V'_{SUB} - (1 + \frac{C_{ox}}{C_{oxb}} + \frac{C_{ox}}{C_{si}})\psi_{s2}(z) + (\frac{C_{ox}}{C_{oxb}} + \frac{C_{ox}}{C_{si}})V'_{GS2}]}{[1 + \frac{2C_{si}}{C_{oxb}}]H_{fin}^2}; \quad (30)$$

Where $C_{ox} = \frac{\epsilon_{HfO2}}{t_{eff}}$; $C_{si} = \frac{\epsilon_{si}}{H_{fin}}$; $C_{oxb} = \frac{\epsilon_{ox}}{t_{oxb}}$; $t_{eff} = t_{SiO2} + \frac{\epsilon_{SiO2}}{\epsilon_{HfO2}} t_{HfO2}$;

Here, the effective oxide thickness (t_{eff}) [24] considered in silicon dioxide thickness (t_{SiO2}) and hafnium dioxide thickness (t_{HfO2}), permittivity of low dielectric (ϵ_{SiO2}), permittivity of high dielectric (ϵ_{HfO2}) and permittivity of silicon (ϵ_{si}).

Substituting all these coefficients in (15), we get:

$$\frac{d^2\psi_{s1}(z)}{dz^2} - \alpha\psi_{s1}(z) = \beta_1; \quad (31.a)$$

$$\frac{d^2\psi_{s2}(z)}{dz^2} - \alpha\psi_{s2}(z) = \beta_2; \quad (31.b)$$

Applying (31), we get $\psi_{s1}(z)$ and $\psi_{s2}(z)$ are:

$$\psi_{s1}(z) = A \exp(\lambda_1 z) + B \exp(\lambda_2 z) - \beta_1/\alpha; \quad (32.a)$$

$$\psi_{s2}(z) = C \exp(\lambda_1(z - L_1)) + D \exp(\lambda_2(z - L_1)) - \beta_2/\alpha, \quad (32.b)$$

From 31(a) and 31(b) the values of α, β_1, β_2 and constants are given in the Appendix A.

In order to attain an ample explanation of adequate the boundary conditions in the middle of the source and drain channel inside the silicon fin at changed distance y from the front-gate. We predictable a relationship between $\psi_{s1}(z)$ and $\psi_y(z)$ within M1 at a height y equivalent to portion n of the H_{fin} [24]. A relationship is obtained by replacing the Y is equal to H_{fin} / n where $n \neq 0$ in (25) between $\psi_{s1}(z)$ and $\psi_y(z)$.

Now, replacing $n=y/H_{fin}$, the potential distribution of the asymmetric DM TFET [25] is attained within M1 as:

$$\psi_{asym1}(y, z) = A_1 \exp(\lambda_{1a} z) + B_1 \exp(\lambda_{2a} z) + \sigma_{asym1} \quad (33)$$

In the same way, the potential distribution of asymmetric DM TFET within M2 as:

$$\psi_{asym2}(y, z) = C_1 \exp(\lambda_{1a}(z - L_1)) + D_1 \exp(\lambda_{2a}(z - L_1)) + \sigma_{asym2}, \quad (34)$$

where $\sigma_{asym1} = -\beta_{asym1}/\alpha_{asym}$, $\sigma_{asym2} = -\beta_{asym2}/\alpha_{asym}$, $\lambda_{1a} = -\sqrt{\alpha_{asym}}$; $\lambda_{2a} = -\sqrt{\alpha_{asym}}$

the values of $\alpha_{asym}, \beta_{asym1}, \beta_{asym2}, A_1, B_1, C_1$ and D_1 are given Appendix B.

Due to the existence of greater work function in M_1 , asymmetric DM TFET minimum potential shall exist i.e., $\psi_{asym,min} = 2\sqrt{A_1 B_1} + \sigma_{asym1}$ (35)

The electric field for asymmetric DM TFET under M1 is computed in z direction as

$$E_{asym1}(y, z) = A_1 \lambda_{1a} \exp(\lambda_{1a}(z)) + B_1 \lambda_{2a} \exp(\lambda_{2a}(z)) \quad (36)$$

Similarly, The electric field for asymmetric DM TFET under M2 in the direction of z is calculated from $d\psi_{asym2}/dz |_{y=0}$, by the following:

$$E_{asym2}(y, z) = C_1 \lambda_{1a} \exp(\lambda_{1a}(z - L_1)) + D_1 \lambda_{2a} \exp(\lambda_{2a}(z - L_1)) \quad (37)$$

4.3 Potential for symmetric DM TFET

The potential for a symmetric DM TFET ($\psi(x, z)$) will be calculated in the same way as asymmetric case, Substitute y for x , H_{fin} for T_{si} , t_{oxb} for t_{ox} , and V_{sub} for V_{gs} .

A symmetric case for potential distribution under M_1 and M_2 are specified as:

$$\psi_{sym1}(x, z) = A_2 \exp(\lambda_{1s}z) + B_2 \exp(\lambda_{2s}z) + \sigma_{sym1} \tag{38}$$

$$\psi_{sym2}(x, z) = C_2 \exp(\lambda_{1s}(z - L_1)) + D_2 \exp(\lambda_{2s}(z - L_1)) + \sigma_{sym2}, \tag{39}$$

At this point $\sigma_{sym1} = -\frac{\beta_{sym1}}{\alpha_{sym}}$, $\sigma_{sym2} = -\frac{\beta_{sym2}}{\alpha_{sym}}$ and $\lambda_{1s} = \lambda_{2s} = \sqrt{\alpha_{sym}}$.

The limits of asymmetric case α_{asym} , β_{asym1} , and β_{asym2} are attained from symmetric case of α_{sym} , β_{sym1} , and β_{sym2} , respectively, by substituting C_{si} for C_T and C_{oxb} for C_{ox} , including the above mention derivation.

Also, the constants A_2 , B_2 , C_2 , and D_2 are attained from A_1 , B_1 , C_1 , and D_1 , respectively, by replacing λ_{1asym} for λ_{1sym} , λ_{2asym} for λ_{2sym} , σ_{asym1} for σ_{sym1} , and σ_{asym2} for σ_{sym2} .

Smearing the condition $d\psi_{sym1}/dz|_{z=0}$ in (38), we attain the minimum potential of symmetric case is: $\psi_{sym,min} = 2\sqrt{A_2 B_2} + \sigma_{sym1}$ (40)

The derivative of symmetric case potential distribution function w.r.to z at limit $z=0$, get the DM TFET electric field component at drain end is

$$E_{sym2}(x, z) = C_2 \lambda_{1s} \exp(\lambda_{1s}(z - L_1)) + D_2 \lambda_{2s} \exp(\lambda_{2s}(z - L_1)) \tag{41}$$

4.4 Potential for the DM Fin-gate TFET

In the DM Fin-gate TFET, the potential distribution is represented as the perimeter-weighted sum of $\psi_{asym1}(y, z)$ and $\psi_{sym1}(x, z)$ underneath of M_1 , and ($\psi_{asym2}(y, z)$ and $\psi_{sym2}(x, z)$) underneath of M_2 , as shown below:

$$\psi_1(x, y, z) = \left(\frac{T_{si}}{T_{si} + 2H_{fin}}\right) \psi_{asym1}(y, z) + \left(\frac{2H_{fin}}{T_{si} + 2H_{fin}}\right) \psi_{sym1}(x, z) \tag{42}$$

$$\psi_2(x, y, z) = \left(\frac{T_{si}}{T_{si} + 2H_{fin}}\right) \psi_{asym2}(y, z) + \left(\frac{2H_{fin}}{T_{si} + 2H_{fin}}\right) \psi_{sym2}(x, z) \tag{43}$$

$$\psi_{S,min} = \left(\frac{T_{si}}{T_{si} + 2H_{fin}}\right) \psi_{asym,min} + \left(\frac{2H_{fin}}{T_{si} + 2H_{fin}}\right) \psi_{sym,min} \tag{44}$$

$$E_F(x, y, z) = \left(\frac{T_{si}}{T_{si} + 2H_{fin}}\right) E_{asym2}(y, z) + \left(\frac{2H_{fin}}{T_{si} + 2H_{fin}}\right) E_{sym2}(x, z), \tag{45}$$

Where $\psi_{S,min}$ is the minimum potential distribution and $E_F(x, y, z)$ is electric field at the drain side.

Based on Kane's method calculate tunnelling current (I_D) [21] which is done by assimilating the BTB generation rate of carriers (G_{BTB}) [22] on the device volume.

In this model we using BTB approach.

$$I_{BTBT} = q \int G_{BTB} dV = q \int \mathcal{A} \frac{|E_F|^G}{E_g^{1/2}} \exp\left(-\mathcal{B} \frac{E_g^{3/2}}{|E_F|}\right) dV. \tag{46}$$

Where $\mathcal{A} = \frac{q^2 \sqrt{2m_{tunnel}}}{h^2 \sqrt{E_g}}$; $\mathcal{B} = \frac{\pi^2 E_g^{3/2} \sqrt{m_{tunnel}/2}}{qh}$; $m_{tunnel} = \frac{m_0 m_e m_h}{m_e + m_h}$;

Where \mathcal{A} and \mathcal{B} are defined by material dependent Kane parameters, band gap materials and effective electron (or) hole mass. Regional and average electrical fields (E_{avg}) [23] are indicated in the E_F component. Here m_0 is the portion of the mass electron and m_e, m_h are the effective mass of electrons and holes.

The current submitted to the Source- tunneling junction underneath M_1 can be described as

$$I_{s-c} = \int_0^{t_{si}} \int_0^{H_{fin}} \int_{Z_{s1}}^{Z_{s2}} \mathcal{A} E_s E_{avg}^{G_1-1} \exp\left(\frac{-B}{E_{avg}}\right) dx dy dz \tag{47}$$

Here Electric field in average (E_{avg}) = $\frac{E_g}{q \cdot I_{s,path}}$ and $E_s = \sqrt{E_{x1}^2 + E_{y1}^2 + E_{z1}^2}$ is the total electric field in region 1 below M_1 at the source channel junction .

$I_{s,tunnel} = Z_{s2} - Z_{s1}$. Present the successful tunneling length at junction of source-channel with Z_{s1} is the distance between tunneling start from source valance band (VB) to channel conduction band (CB) and Z_{s2} is the channel location where tunneling ends.

$$\text{Where } Z_{s1} = \frac{E_g + E_{VS} - E_{FS} - A_1 - B_1 - (H_1/G)}{q\sqrt{G}(A_1 - B_1)} ;$$

(48)

Here E_{VS} and E_{FS} are source VB and Fermi level of source side. Similarly, the total electric field of fin gate TFET (E_D) = $\sqrt{E_{x2}^2 + E_{y2}^2 + E_{z2}^2}$ at region-2 the tunneling at drain-channel junction (i.e., $I_{D,tunnel} = Z_{d2} - Z_{d1}$) is also accountable.

$$\text{Where } Z_{d2} = \frac{E_g + E_{VS} - E_{VC} - A_2 - B_2 - (H_2/G)}{\sqrt{G}(A_2 - B_2)} ;$$

(49)

The current contributions due to carriers tunneling at the junction of Drain-channel underneath M_2 can be described as

$$I_{D-c} = q \int_0^{t_{si}} \int_0^{H_{fin}} \int_{Z_{d1}}^{Z_{d2}} \mathcal{A} E_d E_{avg}^{G_2-1} \exp\left(\frac{-B}{E_{avg}}\right) dx dy dz \tag{50}$$

$$\text{From now, total tunneling current } (I_{tunnel}) = I_{tunnel,S-c} + I_{tunnel,D-c} \tag{51}$$

The tunneling current (I_{tunnel}) from equ.(57) and input voltage (V_{gs}) can be evaluate an Subthreshold swing of device is defined as:

$$\text{Subthreshold swing}(S) = \frac{\partial V_{GS}}{\partial \log I_D} = \left[\frac{\partial \log I_{tunnel}}{\partial V_{GS}} \right]^{-1}$$

(52)

The high speed devices require low SS value. That is the characteristics of the device must be steeper for fast switching of the device. Fast switching from ON to OFF more suitable for low power applications

5.RESULTS DISCUSSION

In this section, based on analytical model derived and the simulated results, we reported the channel potential, electrical field and drain current of proposed device. BTBT current is developed by using the Kane model. To validate the accuracy of our derived model, TCAD simulator [29] data were given. For the simulation of the proposed device SRH recombination model [30] and dynamic barrier tunneling model [31] were supported. We used the device parameters as set out in Table 1. Figure 2 is shown 3D simulated output of the proposed device.

Table 1 Device simulation parameters

Parameter	Values
Doping Concentration of drain side (N_d)	10^{18} cm^{-3}
Doping Concentration of source side (N_s)	10^{20} cm^{-3}
Doping Concentration of Channel (N_{ch})	10^{17} cm^{-3}

Length of the Channel (L)	40nm
Gate metal-1 (Cobalt) work function	4.7ev
Gate metal-2 (Aluminium) work function	4.1ev
Gate oxide (SiO ₂) thickness	3nm
BOX thickness (t _{box})	50nm
Fin width W _{fin} (T _{si})	40nm
Fin height (H _{fin})	20nm
Metal-1&2 length	20nm

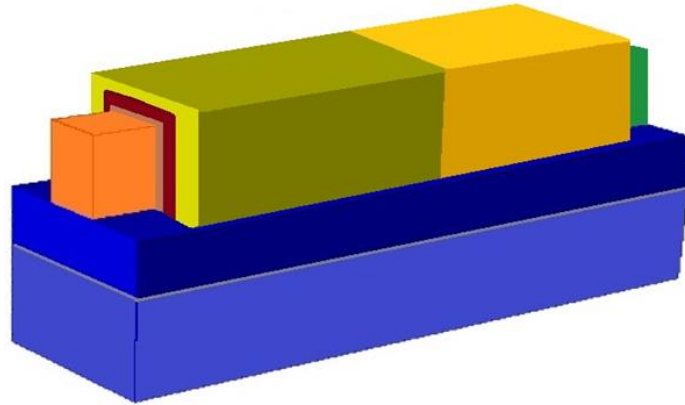


Figure 6. Simulated 3D structure of Dual gate oxide DM Fin TFET structure

5.1 Transfer characteristics

The $I_d - V_{gs}$ characteristics of double metal Fin TFET with work function of metal-1 (Ψ_{M1}) is 4.7 eV, metal-2 (Ψ_{M2}) is 4.1 eV as associated with single metal(SM) gate Fin TFET with double gate oxide is shown in Figure 7. The difference in the drain current with respect to various input bias (V_{gs}) at $V_{ds}=0.05$ V. There is a significant progress in on-state current is 10^{-4} A/m and off state current 10^{-14} A/m in DM Fin TFET and 10^{-6} A/m and off state current 10^{-15} A/m in SM Fin TFET. Therefore, the DMG FinTFET provides improved SS as compared to a conventional SMG FinTFET.

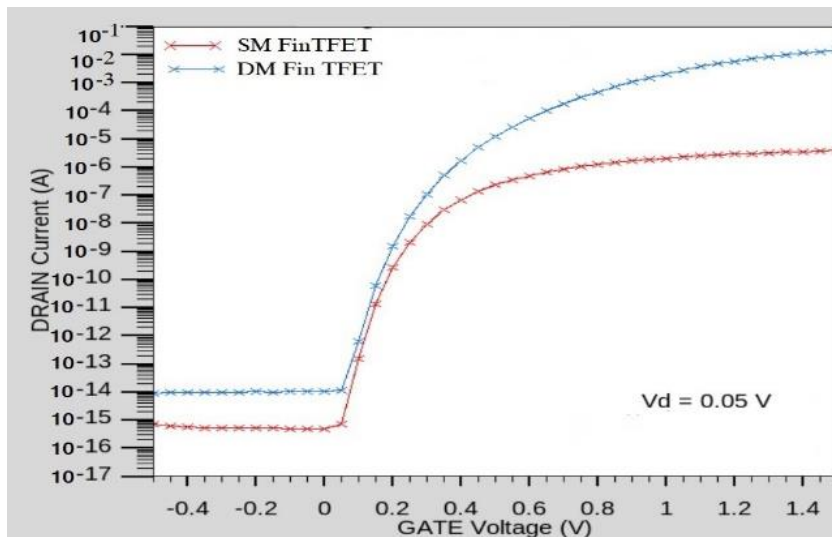


Figure 7. $I_d - V_{GS}$ characteristics of SM Fin TFET and DM Fin TFET.

5.2 Surface potential

In this proposed TFET device dual metal gate arrangement is source side connected to the low work function (Ψ_{M1}) gate material and drain side connected to the high work function (Ψ_{M2}) gate material. Gradual improvement of potential which is tunneling mechanism of drive current at the source and channel junction by use source side lower work function of gate metal. Figure 8. Shows the surface potential of DM Fin TFET compare with SM Fin TFET of Ψ_{M1} (or) Ψ_{M2} is 4.1 eV (or) 4.7eV structures with varying input bias and fixed at drain bias of 0.5 V. However, the use of dual material principle also tends to optimize the OFF state leakage present in the Fin Gate structure.

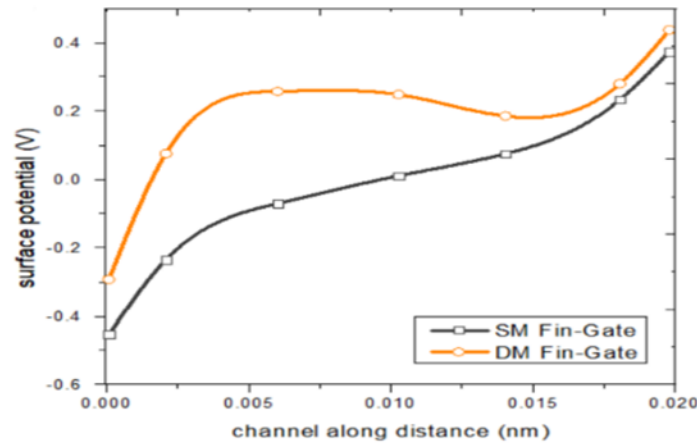


Figure 8. Surface potential distribution along with channel distance at different V_{gs} and $V_{ds}=0.5V$ of SMG and DMG work function (Ψ_{M1} and Ψ_{M2}).

5.3 Total Electric Field

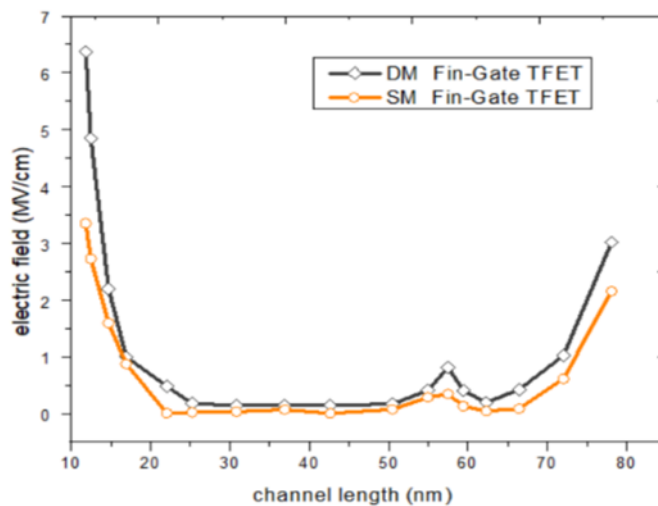


Figure 9. Electric field along the channel distance in SM and DM Fin TFET structures. at $V_{gs}=V_{ds}=0.5V$.

The higher tunneling probability takes place in source – channel junction by use of dual dielectric materials that result higher electric field occurred in source end and also improving device conduction current. Due to the lower electric field, significantly reduce the ambipolar current at the drain end.

Figure 9. represents a contrast of total electric field with regards to channel location for a single metal gate work function of M1 (Ψ_{M1}) has low electric field as compared with double metal gate Ψ_{M1} and Ψ_{M2} of Fin-gate TFET. As compare with source side gate work function is higher than drain side at $V_{gs}=V_{ds}=0.5V$.The tunneling probability of source side junction increase that effected on improving total electric field of DM FinTFET. The device's ambipolar current reduced by negative electric field at drain end which leads to delay the carriers.

Table 2. Comparison of Proposed model with existing models

TFET Structure [Reference]	Device Parameters (units)				
SS ($\frac{mV}{dec}$)	$I_{ON}(\frac{\mu A}{\mu m})$	$I_{OFF}(\frac{\mu A}{\mu m})$	$\frac{I_{ON}}{I_{OFF}}$		
SG TFET Ref.[1]	74	12.1	10^{-4}	10^5	
	Ref.[2]	61.5	10^3	10^{-11}	10^8
DG TFET	Ref.[12]	52	14.8	10^{-10}	10^9
	Ref.[3]	41.2	10^{-8}	10^{-17}	10^{11}
SM Fin TFET	Ref.[6]	25	10^{-6}	10^{-14}	10^8
DM Fin TFET (Proposed model)		21	10^{-4}	10^{-15}	10^{11}

5. Conclusion

This paper proposes analytical modeling of Double Metal Fin gate TFET structure. Surface potential, total electric field and I_{tunnel} are developed on the basis of 3D Poisson equation. As compare with single metal fin gate architecture device has conduction current $10^{-6} \mu A/\mu m$, leakage current $10^{-14} A/m$ and SS value 25 mv/decade, Double gate engineering results in an improved the performance of proposed device in terms of subthreshold slope is 21mv/decade, ON-current is $10^{-4} \mu A/\mu m$ and OFF current $10^{-15} A/m$ is shown in the table 2. The empirical outcomes are in near contract with simulated data from TCAD sentaurus thus confirming our model accuracy.

Conflicts of Interest:

The authors declare that they have no conflicts of interest to report regarding the present study or personal relationships that could have appeared to influence the work reported in this paper.

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Appendix A.

$$\alpha = \frac{2\left(1 + \frac{C_f + C_{si}}{C_b}\right)}{t_{si}^2\left(1 + 2\frac{C_{si}}{C_b}\right)}$$

$$\beta_1 = \frac{qN_A}{\epsilon_{si}} - 2V'_{GS1} \left(\frac{2\left(1 + \frac{C_f + C_{si}}{C_b}\right)}{t_{si}^2\left(1 + 2\frac{C_{si}}{C_b}\right)} \right) - 2V'_{sub} \left(\frac{1}{t_{si}^2\left(1 + 2\frac{C_{si}}{C_b}\right)} \right) ;$$

$$\beta_2 = \frac{qN_A}{\epsilon_{si}} - 2V'_{GS2} \left(\frac{2\left(1 + \frac{C_f + C_{si}}{C_b}\right)}{t_{si}^2\left(1 + 2\frac{C_{si}}{C_b}\right)} \right) - 2V'_{sub} \left(\frac{1}{t_{si}^2\left(1 + 2\frac{C_{si}}{C_b}\right)} \right) ;$$

$$\lambda_1 = \sqrt{\alpha} = \sqrt{\frac{2\left(1 + \frac{C_f + C_{si}}{C_b}\right)}{t_{si}^2\left(1 + 2\frac{C_{si}}{C_b}\right)}} ; \quad \lambda_2 = -\sqrt{\alpha} = -\sqrt{\frac{2\left(1 + \frac{C_f + C_{si}}{C_b}\right)}{t_{si}^2\left(1 + 2\frac{C_{si}}{C_b}\right)}} ;$$

From 32(a) and 32(b) the constants of A, B, C and D values are

$$A = \left\{ \frac{(V_{bi} - \sigma_2 + V_{ds}) - \exp(-\lambda_1(L_1 - L_2)(V_{bi} - \sigma_1)) - (\sigma_1 - \sigma_2)\cos(\lambda_1 L_2)}{1 - \exp(-2\lambda_1(L_1 + L_2))} \right\} \exp(-\lambda_1(L_1 + L_2))$$

$$B = \left\{ \frac{(V_{bi} - \sigma_1) - (V_{bi} - \sigma_2 + V_{ds}) - \exp(-\lambda_1(L_1 + L_2)) - (\sigma_1 - \sigma_2)\cos(\lambda_1 L_2)}{1 - \exp(-2\lambda_1(L_1 + L_2))} \right\} \exp(-\lambda_1(L_1 + L_2))$$

$$C = A \exp(\lambda_1 L_1) + \frac{(\sigma_1 - \sigma_2)}{2}$$

$$D = B \exp(\lambda_2 L_1) + \frac{(\sigma_1 - \sigma_2)}{2}$$

$$\alpha_{asym} = \frac{2\left(1 + \frac{C_{OX}}{C_{OXb}} + \frac{C_{OX}}{C_{Si}}\right)}{\left(H_{fin}^2 \left[\left(1 + \frac{2C_{Si}}{C_{Oxb}} \right) \left(1 + \frac{\epsilon_{si}}{C_{OX}} \right) \right] - \left(1 + \frac{C_{OX}}{C_{OXb}} + \frac{C_{OX}}{C_{Si}} \right) Y^2 \right)}$$

$\beta_{asym1} =$

$$\frac{\left(\frac{qN_A}{\epsilon_{si}} \right) \left(H_{fin}^2 \left[\left(1 + \frac{2C_{Si}}{C_{Oxb}} \right) \left(1 + \frac{\epsilon_{si}}{C_{OX}} \right) \right] - \left(1 + \frac{C_{OX}}{C_{OXb}} + \frac{C_{OX}}{C_{Si}} \right) Y^2 \right) - 2 \left(\frac{C_{OX}}{C_{OXb}} + \frac{C_{OX}}{C_{Si}} \right) V'_{GS1} + V'_{SUB} + \left(\frac{C_{OX}}{\epsilon_{si}} \right) Y (V'_{SUB} - V'_{GS1})}{\left(H_{fin}^2 \left[\left(1 + \frac{2C_{Si}}{C_{Oxb}} \right) \left(1 + \frac{\epsilon_{si}}{C_{OX}} \right) \right] - \left(1 + \frac{C_{OX}}{C_{OXb}} + \frac{C_{OX}}{C_{Si}} \right) Y^2 \right)}$$

$$\beta_{\text{asym}2} = \frac{\left(\frac{qN_a}{\epsilon_{si}} \left(H_{fin}^2 \left[\left(1 + \frac{2C_{si}}{C_{oxb}} \right) \left(1 + \frac{\epsilon_{si}}{C_{ox}} \right) \right] - \left(1 + \frac{C_{ox}}{C_{oxb}} + \frac{C_{ox}}{C_{si}} \right) Y^2 \right) - 2 \left(\left(\frac{C_{ox}}{C_{oxb}} + \frac{C_{ox}}{C_{si}} \right) V'_{GS2} + V'_{SUB} + \left(\frac{C_{ox}}{\epsilon_{si}} \right) Y (V'_{SUB} - V'_{GS1}) \right) \right)}{\left(H_{fin}^2 \left[\left(1 + \frac{2C_{si}}{C_{oxb}} \right) \left(1 + \frac{\epsilon_{si}}{C_{ox}} \right) \right] - \left(1 + \frac{C_{ox}}{C_{oxb}} + \frac{C_{ox}}{C_{si}} \right) Y^2 \right)}$$

$$= \frac{A_1}{1 - \exp(-2\lambda_{1a}(L_1 + L_2))} \left[(V_{bi} - \sigma_{\text{asym}2} + V_{DS}) - \left(\exp(-\lambda_{1a}(L_1 + L_2))(V_{bi} - \sigma_{\text{asym}1}) - ((\sigma_{\text{asym}1} - \sigma_{\text{asym}2})(\cosh(\lambda_{1a}L_2))) \right) \right]$$

$$B_1 = \frac{[(V_{bi} - \sigma_{\text{asym}1}) - (V_{bi} - \sigma_{\text{asym}2} + V_{DS})(\exp(-\lambda_{1a}(L_1 + L_2)) - ((\sigma_{\text{asym}1} - \sigma_{\text{asym}2})(\exp(-\lambda_{1a}(L_1 + L_2))(\cosh(\lambda_{1a}L_2))))]}{1 - \exp(-2\lambda_{1a}(L_1 + L_2))}$$

$$C_1 = \frac{A_1(\exp(\lambda_{1a}L_1)) - (\sigma_{\text{asym}1} - \sigma_{\text{asym}2})}{2};$$

$$D_1 = \frac{B_1(\exp(\lambda_{2a}L_1)) - (\sigma_{\text{asym}1} - \sigma_{\text{asym}2})}{2}$$

Appendix B.

$$\lambda_{\text{sym}} = \sqrt{\frac{\epsilon_{si}t_{ox}W_{fin}}{4\epsilon_{ox}} \left(1 + \frac{\epsilon_{ox}W_{fin}}{\epsilon_{si}4t_{ox}} \right)}; \quad \lambda_{\text{asym}} = \frac{1}{2} \sqrt{\frac{\epsilon_{si}t_{oxb}H_{fin}(2\epsilon_{si}t_{ox} + H_{fin})}{\epsilon_{ox}[\epsilon_{si}(t_{ox} + t_{oxb}) + \epsilon_{ox}H_{fin}]}}$$

$$A(\lambda) = \frac{e^{\frac{4L}{\lambda}} - 2e^{\frac{2L}{\lambda}} + 1}{\left(e^{\frac{L}{\lambda}} - 1 \right)^4}; \quad B(\lambda) = \frac{2e^{\frac{3L}{\lambda}} - 4e^{\frac{2L}{\lambda}} + 2e^{\frac{L}{\lambda}}}{\left(e^{\frac{L}{\lambda}} - 1 \right)^4}; \quad C(\lambda) = \frac{2e^{2\lambda} \left(1 + e^{\lambda} \right)}{\left(e^{\lambda} - 1 \right)^2};$$

$$K_1 = \frac{\epsilon_{si}t_{oxb}}{\epsilon_{si}(t_{ox} + t_{oxb}) + \epsilon_{ox}H_{fin}}; \quad K_2 =$$

$$\frac{[q(\epsilon_{si}/\epsilon_{ox})N_a t_{ox} t_{oxb} H_{fin}] + [\epsilon_{si} \Phi_{ms}(t_{ox} + t_{oxb}) - \epsilon_{ox}(H_{fin} V_{gsb} - \Phi_{ms} H_{fin})] \left[\epsilon_{si} t_{ox} V_{gsb} - \frac{1}{2} q N_a H_{fin}^2 t_{oxb} \right]}{\epsilon_{si}(t_{ox} + t_{oxb}) + \epsilon_{ox}H_{fin}}$$

$$A(\lambda_{\text{asym}}) = \frac{e^{\frac{4L}{\lambda}} - 2e^{\frac{2L}{\lambda}} + 1}{\left(e^{\frac{L}{\lambda}} - 1 \right)^4} \left(\frac{1}{2} \sqrt{\frac{\epsilon_{si}t_{oxb}H_{fin}(2\epsilon_{si}t_{ox} + H_{fin})}{\epsilon_{ox}[\epsilon_{si}(t_{ox} + t_{oxb}) + \epsilon_{ox}H_{fin}]}} \right);$$

$$B(\lambda_{\text{asym}}) = \frac{2e^{\frac{3L}{\lambda}} - 4e^{\frac{2L}{\lambda}} + 2e^{\frac{L}{\lambda}}}{\left(e^{\frac{L}{\lambda}} - 1 \right)^4} \left(\frac{1}{2} \sqrt{\frac{\epsilon_{si}t_{oxb}H_{fin}(2\epsilon_{si}t_{ox} + H_{fin})}{\epsilon_{ox}[\epsilon_{si}(t_{ox} + t_{oxb}) + \epsilon_{ox}H_{fin}]}} \right);$$

$$C(\lambda_{\text{asym}}) = \frac{2e^{2\lambda} \left(1 + e^{\lambda} \right)}{\left(e^{\lambda} - 1 \right)^2} \left(\frac{1}{2} \sqrt{\frac{\epsilon_{si}t_{oxb}H_{fin}(2\epsilon_{si}t_{ox} + H_{fin})}{\epsilon_{ox}[\epsilon_{si}(t_{ox} + t_{oxb}) + \epsilon_{ox}H_{fin}]}} \right);$$

Appendix C.

$$G_1 = A(\lambda_{\text{sym}}) = \frac{e^{\frac{4L}{\lambda}} - 2e^{\frac{2L}{\lambda}} + 1}{\left(e^{\frac{L}{\lambda}} - 1 \right)^4} \left(\sqrt{\frac{\epsilon_{si}t_{ox}W_{fin}}{4\epsilon_{ox}} \left(1 + \frac{\epsilon_{ox}W_{fin}}{\epsilon_{si}4t_{ox}} \right)} \right);$$

$$G_2 = B(\lambda_{\text{sym}}) = \frac{2e^{\frac{3L}{\lambda}} - 4e^{\frac{2L}{\lambda}} + 2e^{\frac{L}{\lambda}}}{\left(e^{\frac{L}{\lambda}} - 1 \right)^4} \left(\sqrt{\frac{\epsilon_{si}t_{ox}W_{fin}}{4\epsilon_{ox}} \left(1 + \frac{\epsilon_{ox}W_{fin}}{\epsilon_{si}4t_{ox}} \right)} \right);$$

$$G_3 = C(\lambda_{\text{sym}}) = \frac{2e^{2\lambda} \left(1 + e^{\lambda} \right)}{\left(e^{\lambda} - 1 \right)^2} \left(\sqrt{\frac{\epsilon_{si}t_{ox}W_{fin}}{4\epsilon_{ox}} \left(1 + \frac{\epsilon_{ox}W_{fin}}{\epsilon_{si}4t_{ox}} \right)} \right);$$

$$H_1 = \frac{A(\lambda_{\text{asym}})}{K_1} = \left[\left(\frac{e^{\frac{4L}{\lambda}} - 2e^{\frac{2L}{\lambda}} + 1}{\left(e^{\frac{L}{\lambda}} - 1\right)^4} \right) \left(\frac{1}{2} \sqrt{\frac{\varepsilon_{\text{si}} t_{\text{oxb}} H_{\text{fin}} (2\varepsilon_{\text{si}} t_{\text{ox}} + H_{\text{fin}})}{\varepsilon_{\text{ox}} [\varepsilon_{\text{si}} (t_{\text{ox}} + t_{\text{oxb}}) + \varepsilon_{\text{ox}} H_{\text{fin}}]}} \right) \left(\frac{\varepsilon_{\text{si}} (t_{\text{ox}} + t_{\text{oxb}}) + \varepsilon_{\text{ox}} H_{\text{fin}}}{\varepsilon_{\text{si}} t_{\text{oxb}}} \right) \right];$$

$$H_2 = \frac{B(\lambda_{\text{asym}})}{K_1} = \left[\left(\frac{2e^{\frac{3L}{\lambda}} - 4e^{\frac{2L}{\lambda}} + 2e^{\frac{L}{\lambda}}}{\left(e^{\frac{L}{\lambda}} - 1\right)^4} \right) \left(\frac{1}{2} \sqrt{\frac{\varepsilon_{\text{si}} t_{\text{oxb}} H_{\text{fin}} (2\varepsilon_{\text{si}} t_{\text{ox}} + H_{\text{fin}})}{\varepsilon_{\text{ox}} [\varepsilon_{\text{si}} (t_{\text{ox}} + t_{\text{oxb}}) + \varepsilon_{\text{ox}} H_{\text{fin}}]}} \right) \left(\frac{\varepsilon_{\text{si}} (t_{\text{ox}} + t_{\text{oxb}}) + \varepsilon_{\text{ox}} H_{\text{fin}}}{\varepsilon_{\text{si}} t_{\text{oxb}}} \right) \right];$$

$$H_3 = \frac{C(\lambda_{\text{asym}})}{K_1} = \left[\left(\frac{2e^{\frac{L}{2\lambda}} (1 + e^{\frac{L}{\lambda}})}{\left(e^{\frac{L}{\lambda}} - 1\right)^2} \right) \left(\frac{1}{2} \sqrt{\frac{\varepsilon_{\text{si}} t_{\text{oxb}} H_{\text{fin}} (2\varepsilon_{\text{si}} t_{\text{ox}} + H_{\text{fin}})}{\varepsilon_{\text{ox}} [\varepsilon_{\text{si}} (t_{\text{ox}} + t_{\text{oxb}}) + \varepsilon_{\text{ox}} H_{\text{fin}}]}} \right) \left(\frac{\varepsilon_{\text{si}} (t_{\text{ox}} + t_{\text{oxb}}) + \varepsilon_{\text{ox}} H_{\text{fin}}}{\varepsilon_{\text{si}} t_{\text{oxb}}} \right) \right];$$