

New and Mechanical Properties of Self-Compacting Microstructure of Lightweight Total Cement with and without Filaments

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Article Info

Page Number: 618 - 623

Publication Issue:

Vol 70 No. 2 (2021)

Article History

Article Received: 05 September 2021

Revised: 09 October 2021

Accepted: 22 November 2021

Publication: 26 December 2021

Abstract

The rising volume of waste tires over the past few years has made them a major environmental concern. Cement can be repurposed in creative ways. Piece tires are broken down into small particles and added to lightweight total cement to make self-compacting elastic lightweight total cement (SCRLC). A lot of testing has been done to see how elastic particles affect the properties of SCRLC and the mortar that goes with it. The plastic thickness and yield pressure both rise when elastic particles are used in mortar. An increase in SCRLC's elastic particle replacement percentage results in a decrease in flowability, filling limit, and passing capacity. There was a close correlation between the SCRLC droop stream, shear pressure, SCRLC isolation percentage, and plastic thickness of the mortar glues in question. To ensure that elastic lightweight total cement can pack on its own, the plastic thickness should be limited to 231.7 Pa with a lower cutoff of 3.72 Pa S. When the elastic particle replacement fraction rises, both SCRLC and the matching mortar experience a decrease in their compressive strengths. For elastic particles, the 28-day compressive strength of SCRLC may meet the requirements for light weight total significant improvements up to a half swap percentage.

1. INTRODUCTION

When waste from the automobile industry, like rubber waste, which has been on the rise recently, is not properly managed, it causes problems for the environment [1]. Rubber waste can be disposed of in a number of different ways. One way to deal with discarded tires might be to use recycled rubber as an aggregate in concrete [2]. Using a lot of rubber in concrete can be a sustainable way to concrete a lot of rubber waste [3,4]. In terms of research, numerous studies have examined the effect that rubber particles have on the physical properties of concrete. There is evidence to suggest that the majority of recycling techniques involve crushing used rubber tires into various sizes and

reusing those sizes in concrete. The workability [5–8], mechanical properties [9, 10], lifespan [11, 12], and application of standard concrete with rubber particles as a material were then examined in greater depth. At the same time, rubber particles were also used in lightweight aggregate concrete.

In recent years, rubber lightweight aggregate concrete (RLC) has been favored over standard rubber concrete due to its low unit weight, high flexibility, and adequate mechanical properties. Additionally, a potential application is on the horizon. However, it is challenging to evenly distribute rubber and aggregate particles throughout the concrete due to their lightness. Consequently, RLC's characteristics are not uniform. Self-compacting technology can be used to correct the uneven distribution of aggregate and rubber particles in RLC, just like it can with concrete. In contrast, there has been little or no previous research on self-compacting rubber lightweight aggregate concrete (SCRLC). It was found that the properties of freshly formed concrete and hardened concrete are very similar. Therefore, it is necessary to investigate the concrete's physical properties right away. It has been demonstrated by researchers that the workability of concrete is directly related to the rheological properties of its mortar [20]. Consequently, mortar's rheological properties can be used to predict a concrete's workability. Consequently, preparing outstanding new SCRLC qualities is made easier by comprehending the matching mortar's rheological characteristics. However, only a few studies have examined the relationship between SCRLC's fresh qualities and mortar's rheological characteristics and the effects of rubber particles on these properties. On the other hand, neither SCRLC nor its mortar counterpart have had their mechanical properties studied.

In this investigation, the self-compacting method was tested to see if it could be used to create RLC with exceptional performance. The fresh and mechanical properties of SCRLC and the mortar that matched it were tested in a number of studies to see how rubber particles affected the results. There are six distinct mixtures in the SCRLC's mix configurations. In the six mixtures, rubber particles of the same size distribution were used to replace the fine aggregate, and replacement volumes ranged from 0% to 50%. The characteristics of the mortar include yield stress, plastic viscosity, and compressive strength. The mechanical properties of SCRLC are evaluated using a variety of approaches, including slip flow, V-funnel, and L box tests. The qualities of SCRLC are also evaluated using the compressive strength and column segregation tests. The relationship between the respective mortar's rheological property characteristics and new SCRLC property findings was also studied. As a result, a better understanding of the factors that influence SCRLC characteristics was concluded.



Fig.1 Crushed shale ceramsite.

2. LITERATURE REVIEW

Materials used in this study were found to be primarily composed of fly debris and common Portland concrete. The solution's formulation also included elastic particles, a water-reducing agent, a thickener, and water. Using a Bruker D8 Advance X-ray diffractometer, an X-ray fluorescence spectrometer was used to examine a mixture of concrete and fly debris.

The improvement company's product has a water retention limit of 2.3%, a compressive strength of 8.82 MPa, a free mass density of 842 kg/m³, and a range of particle sizes from 4.75 to 19 mm. We were instructed by the manufacturer to substitute elastic particles (shown in Figure 2) for sand in order to reduce the volume of the finished product. By multiplying its density (1.19) grams per cubic centimeter by its modulus of fineness (2.7), its free mass was determined. Figure 3 depicts the sizing of elastic particles and sand.

"The water-reducing agent was a high-range water reducer (HRWR) based on polycarboxylates with a 40% active ingredient. National Starch Industry (Shanghai) Co., Ltd. produced the thickener, hydroxypropyl methyl cellulose ether, with a viscosity of 20,000 MPa. Ordinary city water was used in the mixing process.

Proportions and a Methodology in Congruence In this research project, the freshness and mechanical properties of SCRLC and a mortar that matched it were examined. Table 2 shows the proportions of the SCRLC mixture. A ratio of 1.00 exists: Cement; 0.20:0.012.42 ash fly; FA; thickener; LWA; HRWR; water) in the mix used as a control This work substituted rubber particles for sand, with replacement rates ranging from 10% to 50%. To keep SCRLC working, a thickener and water-reducing agent were used. SCRLC The formula contained a water-reducing agent of 1% and a thickener of 0.04 percent (by weight of binding materials). The ratio of water to binding materials was set at 0.42. Concrete compositions devoid of lightweight aggregate served as the basis for the proportions of the mixture.

The water-reducing agent and thickening agent were added to the dry mixture that had been kneaded for the first minute after being mixed for two minutes. After mixing, the rheological properties of the mortar paste were immediately tested at 20 °C. Before being added to the concrete, the dry-mixed components—cement, fly ash, rubber particles, sand, and light-weight aggregate—were first mixed for a minute. The thickening and thinner were incorporated after two more minutes of high speed mixing. Molds were loaded with mastic paste and a self-compacting lightweight agglomerate, and then baked for 24 hours to produce two distinct sets of parts. Following the pre-tests, slump flow, the L-box, the V-funnel, the U-box, and column segregation were tested immediately in a controlled environment at 20 °C. Before each sample was tested, it was kept at 20 °C and at least 95% relative humidity for 7, 28, and 90 days, respectively. After that, SCRLC and hardening mortar's mechanical properties were tested.

Between 0 S1 and 40 S1, the results of a rheological test revealed a linear increase and decrease in shear rate. The rheological properties of the flow curves were examined using the descending portion. The Bingham model, which is based on previous research, has previously been used to characterize the rheological properties of a cement paste. As a result, in the hope that the Bingham model would be useful, the rheological properties of mortar containing rubber particles were studied using it. To determine the plastic viscosities and yield stress, employ the Bingham model as shown below.

Tests of Mechanical Properties In this study, the mechanical properties of a mortar and SCRLC hardening were tested. SCRLC's compressive, tensile, flexural, and elastic modulus strengths were evaluated in a number of studies. At this time, mortar was tested for its compressive strength. 100 mm-diameter cubic specimens were used to test the SCRLC's compressive and splitting tensile strengths. By measuring the elastic modulus of a prismatic specimen that met the requirements of the GB/T 50081 standard, it was determined that SCRLC had an elastic modulus of 100 100 300 mm. The flexure strength of SCRLC was measured with prismatic specimens that were 100, 400, and 1000 mm in size. The compressive strength of mortar was measured using three specimens, each with a cubic volume of 70,7,7,7 mm, in accordance with JGJ/T 70. No specimens had to be compacted for mechanical characteristics testing. For these tests, we made use of computer-operated universal testing equipment. understanding and comparing SCRLC's compressive, splitting-tensile, and flexural strengths to cor's compressive strengths



Fig.2 Sump flow test

3. PROPOSED SYSTEM

The design of the V-Funnel was put to the test. Time required for a V-funnel flow The value of T_v varies depending on the rubber particle replacement ratio in Figure 15. As can be seen in the figure, the rate at which rubber particles are replaced is higher. T_v increases from 14.7 to 24.3 seconds, or roughly 66%, depending on the various rubber particle replacement ratios (0–50 percent). It demonstrates that the new SCRLC's filling capacity decreases when the rubber particle replacement ratio increases. Because rubber particles don't absorb water, they add more water to concrete mixtures, which makes the finished product more fluid.

For the test, make use of an L-Box. Figure 16, which depicts the combined results, combines the T400 and h_2/h_1 findings. T400 goes up when rubber particle replacement goes up, but h_2/h_1 goes down. Rubber particles increase T400 from 7.7 to 10.9 seconds with a replacement ratio of 0 to 50% while decreasing the h_2/h_1 ratio from 0.98 to 0.82 seconds. The T400 and h_2/h_1 variations demonstrate that as the replacement ratio of rubber particles rises, the passage capacity of fresh SCRLC decreases. Shape and surface properties of rubber particles may also have an effect on fresh SCRLC



Fig.3 Proposed Methodology

4. CONCLUSION

In this study, numerous tests were carried out to determine how SCRLC differed from mortars of the same composition. The findings of our investigation can be found below. The Bingham model can be used to model shear rates and stresses for mortar pastes with varying rubber particle replacement ratios. By adding more rubber particles to the mortar, mortar pastes can be made much better. The molding properties of the finished product suffer when the proportion of rubber particles in the mortar increases. The fresh characteristics of the SCRLC, such as the diameter of the slump flow, the h_2/h_1 ratio, and the segregation ratio, are diminished when rubber particles are replaced in the SCRLC. As the proportion of rubber replacement particles rises, SCRLC's ability to flow, fill, and pass decrease. As the rubber particle replacement ratio rises, SCRLC segregation resistance rises significantly. The new features of SCRLC and the rheological properties of mortar paste are clearly linked. The mortar pastes must have a plastic viscosity of less than 3.72 Pa and a shear tension of less than 231.7 Pa, respectively.

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